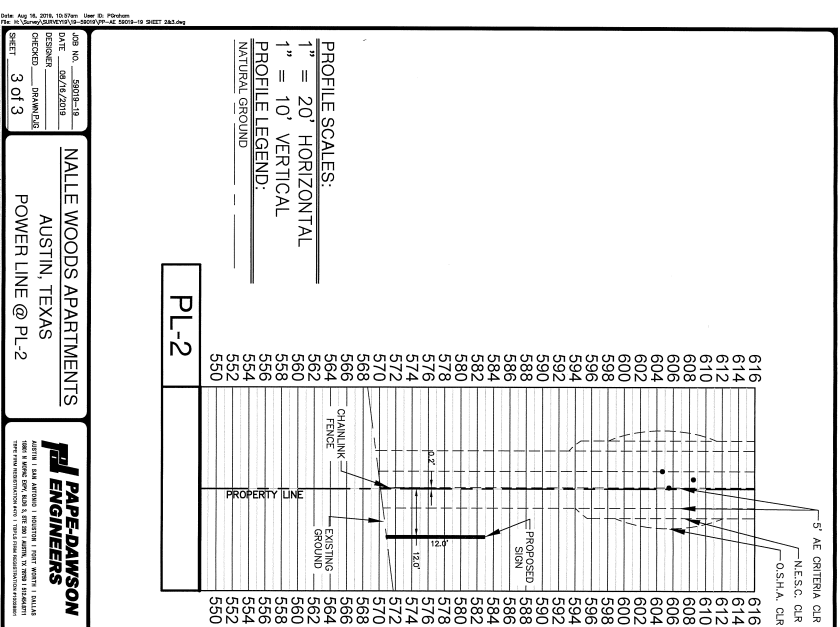
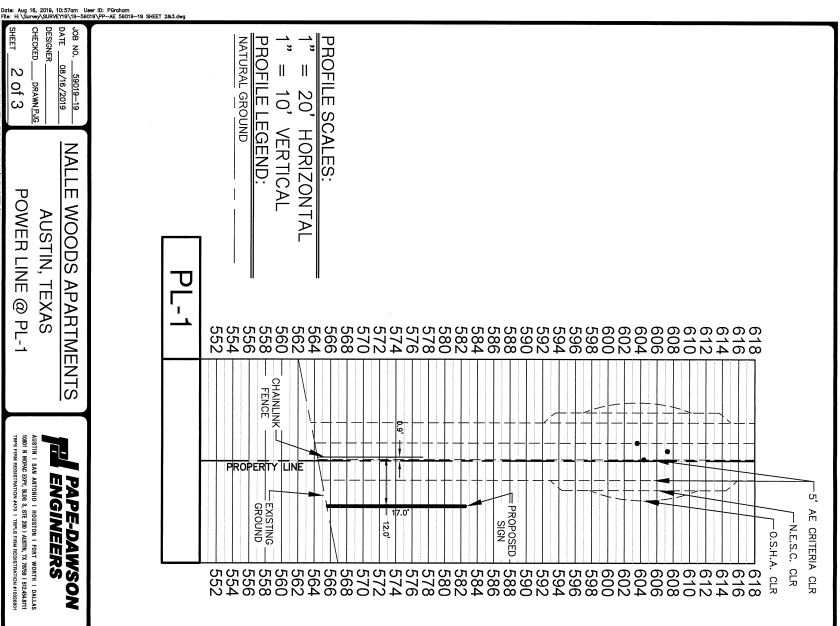
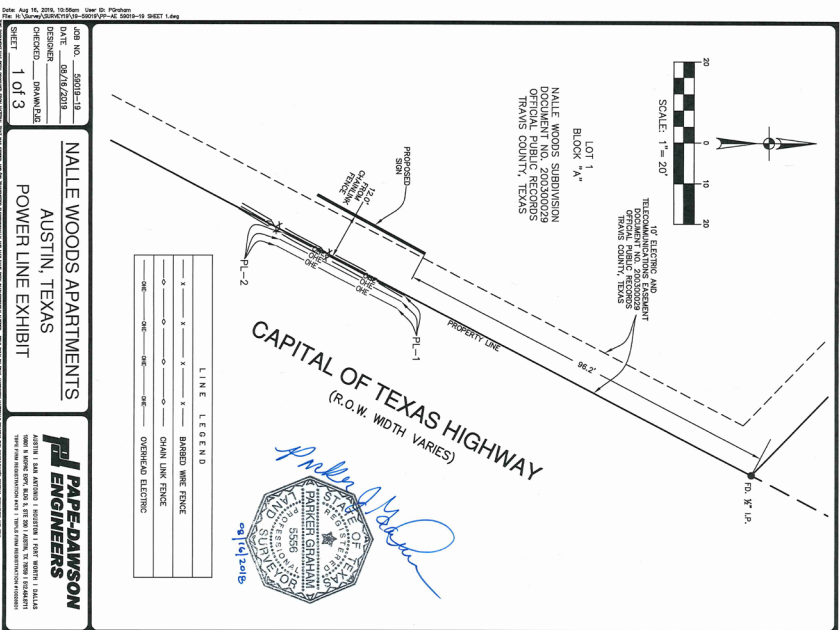


**EXHIBIT 14 - TOPOGRAPHY OF LAND AND TREES**



**NALLE WOODS**  
4700 N Capital of Texas Hwy.,  
Loop 360  
Austin, TX 78746

# Sign Variance Request



## Overhead View

## Northside of Sign

## Southside of Sign

EXHIBIT 16 - ENGINEER DRAWING OF SIGN STRUCTURE - SULLAWAY ENGINEERING

1 of 4

**C-1/47**

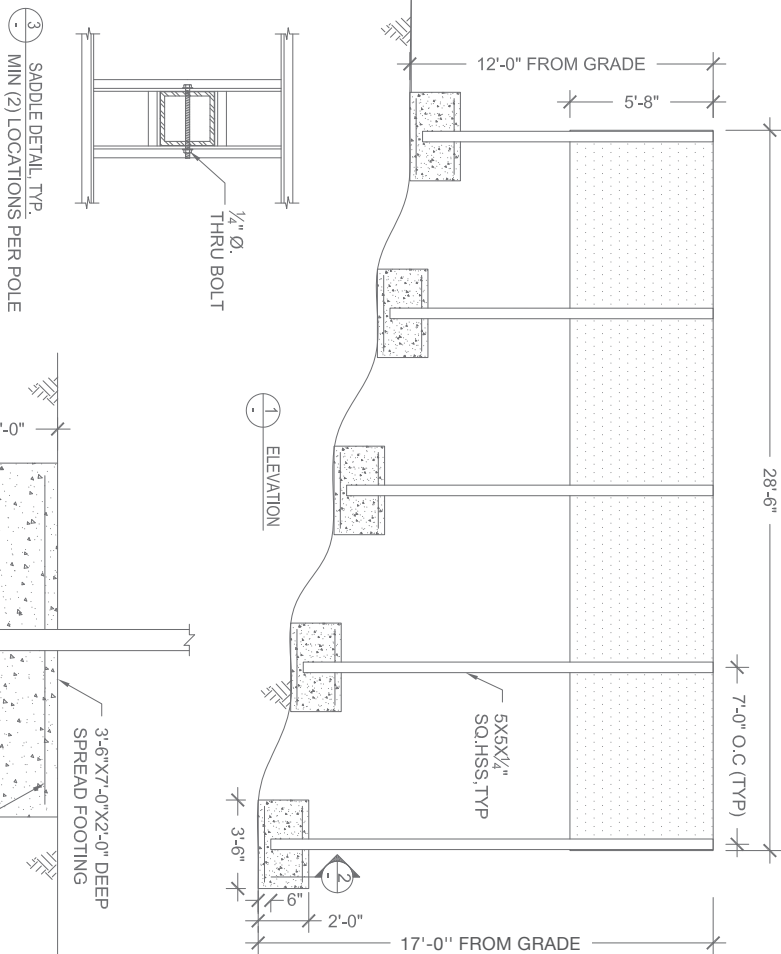
**NALLE WOODS**  
4700 N Capital of Texas Hwy.,  
Loop 360  
Austin, TX 78746

**SULLAWAY**  
**ENGINEERING**

10815 RANCHO BERNARDO RD., SUITE 200  
SAN DIEGO, CA 92198  
PHONE: 1-858-312-5150 FAX: 1-858-777-3334

PROJECT: NALLE WOODS, 4700 N CAPITAL OF TEXAS HWY, AUSTIN, TX  
PROJECT #: 22688  
CLIENT: MELLO SIGNS

DATE: 08-09-2019  
ENGINEER: PS  
LAST REVISED:



- GENERAL NOTES
1. DESIGN CODE: IBC 2015
  2. DESIGN LOADS: ASCE 7-10
  3. WIND VELOCITY: 115 MPH EXPOSURE C
  4. CONCRETE: 2500 PSI MINIMUM
  5. SQ./RECT. HSS STEEL: ASTM A500 GR. B, F<sub>y</sub> = 46 KSI MIN.
  6. BOLT: STEEL: ASTM A307, HDG PER ASTM A153, 2P PER ASTM B633
  7. STEEL REINFORCEMENT IN CONCRETE: ASTM A615 GR 60
  8. PROVIDE MIN. 3" CLEAR COVER ON ALL STEEL EMBEDDED IN CONCRETE WHEN CAST AGAINST SOIL
  9. VERTICAL SOIL BEARING PER IBC CLASS 4 (2000 PSF)
  10. PROVIDE PROTECTION AGAINST DISSIMILAR METALS
  11. ALL DIMENSIONS TO BE VERIFIED PRIOR TO FABRICATION



EXHIBIT 16 CONT. - ENGINEER DRAWING OF SIGN STRUCTURE - SULLAWAY ENGINEERING

NALLE WOODS  
4700 N Capital of Texas Hwy.,  
Loop 360  
Austin, TX 78746

SIGN VARIANCE REQUEST



10815

PROJECT: NALLE WOODS  
PROJ. NO.: 22688  
CLIENT: MELLO SIGNS

DATE: 8/9/19  
ENGINEER: PS

Applied Wind Loads: from ASCE 7-10

$F=q_z \cdot G \cdot C_f \cdot A_f$  with  $q_z = 0.00256 K_z K_d V^2$  (29.3.2 & 29.4)

$C_f = 1.793$  (Fig. 29.4-1)

$K_d = 1.0$  (26.6.2) (=1.0 unless unusual landscape)

$K_z =$  from table 28.3-1

$K_d = 0.85$  for signs (table 26.6-1)

$V = 115$  mph

$G = 0.85$  (26.9)

$s/h = 0.315$

$B/s = 5.03$

weight= 0.448 kips

$M_{wz} = 0.00$  k-ft

| Pole Loads | structure component | height at section c.g. | $K_z$ | $q_z$ | pressure $q_z \cdot G \cdot C_f$ | $A_f$ | shear | Wind Moment $M_w$ |
|------------|---------------------|------------------------|-------|-------|----------------------------------|-------|-------|-------------------|
| 1          | 6.16666667          | 0.85                   | 24.5  | 37.3  | 5.1                              | 192   | 1181  |                   |
| 2          | 13.66666667         | 0.85                   | 24.5  | 37.3  | 18.7                             | 696   | 9508  |                   |
| 3          | 16.5                | 0.87                   | 24.9  | 38.0  | 21.0                             | 797   | 13158 |                   |

$P_u = 0.54$  kip

$M_u = \text{sqrt}(1.2 M_{Dz}^2 + 1.0 M_{wz}^2) = 23.85$  k-ft  $M = 23.85$  k-ft  $M = \text{sqrt}(M_{Dz}^2 + M_{wz}^2)$  arm= 14.2

Pole Design

section: tube

| $M_u \leq \phi M_n$ , with $M_n = f_y Z$ | $f_y$        | 46 ksi        | $\phi = 0.9$ | Z      | Use                                          |
|------------------------------------------|--------------|---------------|--------------|--------|----------------------------------------------|
| H                                        | $M_u$ (k-ft) | Z req'd. (in) | Size (in)    | t (in) |                                              |
| at grade                                 | 23.85        | 6.91          | 5            | 0.233  | 7.6 5X5x1/4" SQ. HSS, $\phi M_n = 26.2$ k-ft |



P.O.

1501 fax: 555/775354

PROJECT: NALLE WOODS  
PROJ. NO.: 22688  
CLIENT: MELLO SIGNS

DATE: 8/9/19  
ENGINEER: PS

V&O

Longitude Direction

applied shear at grade  $V = 1.053$  kip

applied moment at grade  $m = 14.904$  kip-ft

depth of soil above footing  $h_s = 0.0$  ft

allowable soil bearing  $p = 2.600$  ksf (i.e.,  $2000 \times 1.33 = 2660$  psf)

(use a factor of 1.33 for wind or seismic)

Spread Footing Design

moment  $m = 17.0$  k-ft

Footing size (ft)  $b = 3.50$

Footing Weight= 7.4 k

Overturning:  $M_o = 27$

soil pressure: max= 1.126 ksf

forces on concrete pad:  $V = 8$  k

$M = 13$  k-ft

Check Slab:

Flexure  $A_s = 0.25$

$\phi M_n = \phi A_s f_y (d - a/2) = 269$  k-in

$a = A_s f_y / 0.85 f'_c b = 0.168$  in

Check minimum  $A_{smin} = 3 \text{sqrt}(f'_c) b d f_y = 2.1$

ACI 10.3.1

short direction  $\gamma_s = 2 / (b + 1) = 0.8$  with  $\beta = 1.5$

Use  $A_s = 0.33$  in<sup>2</sup>  $\gamma A_s = 0.27$  in<sup>2</sup> use #4@12" each direction

Shear:  $\phi V_n = \phi 2 \text{sqrt}(f'_c) b d \quad \phi V_c = 63.0$

$\phi = 0.75$

$V < \phi V_n$  OK

Top Slab

Assume half of footing is in uplift

weight= 4 kip

$M = 6$  k-ft

Flexure  $A_s = 0.150$

$\phi M_n = \phi A_s f_y (d - a/2) = 162$  k-in

$a = A_s f_y / 0.85 f'_c b = 0.050$  in

Check minimum  $A_{smin} = 2 \text{sqrt}(f'_c) b d f_y = 4.2$

short direction  $\gamma_s = 2 / (b + 1) = 0.8$  with  $\beta = 1.5$

Use  $A_s = 0.20$  in<sup>2</sup>  $\gamma A_s = 0.16$  in<sup>2</sup> use #4@12" each direction

$M < \phi M_n$  OK  $2000 b d f_y = 5.60$  or  $1.333 A_s = 0.2$  in<sup>2</sup>